# A Finite Volume Scheme for the Transport of Radionucleides in Porous Media

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1. Physical problems, engineering methods

- 2. Application to a simplified case
- 3. Numerical results
- 4. Concluding remarks



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## **Physical problems**

Transport of mass and energy within porous media :

- Pollution of soils

- ...

- Degradation of concrete
- Migration of hydrocarbon components



## **Examples of conservation equations in porous media**

 $N^c$  components,  $N_p$  phases

$$(A_p^c)_t + \operatorname{div} F_p^c = R_p^c$$

$$A_p^c = S_p \xi_p X_p^c$$

$$F_p^c = \xi_p X_p^c V_p - D_p^c (V_p) \cdot \nabla X_p^c$$

$$D_p^c(v) \cdot w = a_p^c w + |v| \left( b_p^c \frac{v \cdot w}{v \cdot v} v + c_p^c (w - \frac{v \cdot w}{v \cdot v} v) \right)$$

$$V_p = -K \frac{k_{rp}(S_p)}{\mu_p} (\nabla P_p - \rho_p g)$$



## **Mathematical questions**

**Existence and uniqueness of solutions** 

Numerical approximation

**Convergence and error estimates** 

Austin, March 2003

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# **Approximation using finite volume methods**

**Conservation equation** 

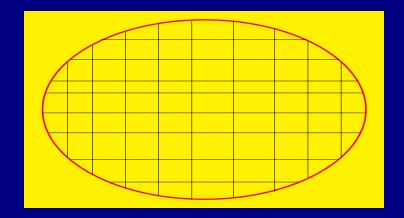
$$\frac{\partial A}{\partial t} + \operatorname{div} \mathbf{F} = R$$

with

- *A* : extensive quantity
- F : flux
- R : reaction term

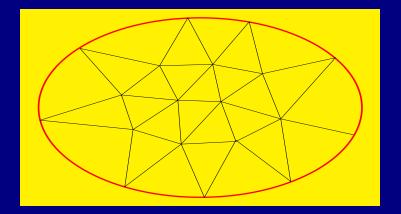


## Partition of the domain



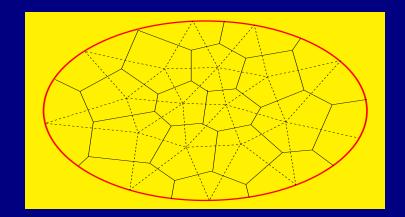


## Partition of the domain





## Dual mesh (Voronoï mesh)





#### **Extensive balance in control volumes**

$$m_{K} \frac{A_{K}^{(n+1)} - A_{K}^{(n)}}{\delta t^{(n)}} + \sum_{L \in \mathcal{N}_{K}} F_{K,L}^{(n,n+1)} = m_{K} R_{K}^{(n)}$$

$$F_{K,L}^{(n,n+1)}$$
 approx.  $\frac{1}{\delta t^{(n)}} \int_{t^{(n)}}^{t^{(n+1)}} \int_{K|L} \mathbf{F} \cdot \mathbf{n}_{K,L} ds dt$ 

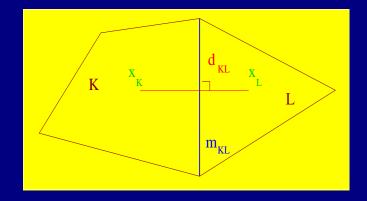
 $F_{K,L}^{(n,n+1)} = -F_{L,K}^{(n,n+1)} \Rightarrow \text{local conservation}$ 



## **Flux approximation**

Finite Difference Approximation of  $\mathbf{F} = -a \nabla u$ 

$$F_{K,L} = -a \ m_{KL} \frac{u_L - u_K}{d_{KL}}$$





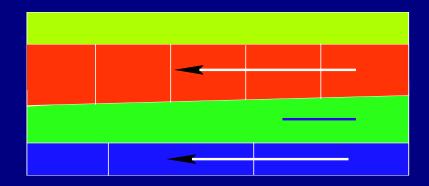
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## The COUPLEX 1 case

$$div V_1 = 0 \text{ with } V_1 = -K(\nabla P_1 - \rho_1 g)$$
$$(X_1^1)_t - div \left( \begin{array}{c} X_1^1 V_1 - D(V_1) \cdot \nabla X_1^1 \end{array} \right) = -\Lambda X_1^1$$



#### Finite volume scheme on Voronoï mesh

$$H_{K} = P_{1K} - \rho_{1}g \cdot z_{K} \text{ and } V_{K,L} = m_{KL}\frac{H_{K} - H_{L}}{d_{KL}}$$
  
FV scheme: 
$$\sum_{L \in N_{K}} V_{K,L} = 0$$

$$\frac{m_{KL}}{d_{KL}} = -\int_{\Omega} \nabla \varphi_K(x) \cdot \nabla \varphi_L(x) dx \quad \Rightarrow \mathbf{FV} = \mathbf{FE}$$

approx.  $\nabla H$  constant by triangle

#### **Finite volume scheme for concentrations**

$$m_{K} \frac{X_{K}^{(n+1)} - X_{K}^{(n)}}{\delta t} + \sum_{L \in N_{K}} \begin{bmatrix} X_{K,L}^{(m)} V_{K,L} - \\ D_{KL} (X_{L}^{(m)} - X_{K}^{(m)}) \end{bmatrix} = m_{K} (R_{K}^{(n)} - k X_{K}^{(n+1)})$$

with

$$D_{KL} = -\int_{\Omega} \nabla \varphi_K(x) D(\nabla H) \nabla \varphi_L(x) dx$$
$$m = n \text{ or } m = n + 1$$



## **Upwinding scheme**

$$\begin{array}{ll} \text{if } V_{K,L} \geq 0 \quad \text{ then } \quad X_{K,L}^{(m)} = X_K^{(m)} \\ \text{ else } \quad X_{K,L}^{(m)} = X_L^{(m)} \end{array}$$



#### Variable Péclet number finite volume scheme

$$X_{K,L}^{(m)} = \theta_{K,L} X_K^{(m)} + (1 - \theta_{K,L}) X_L^{(m)}$$
  

$$\Rightarrow F_{K,L}^{(m)} = \left(\theta_{K,L} X_K^{(m)} + (1 - \theta_{K,L}) X_L^{(m)}\right) V_{K,L} - D_{KL} (X_L^{(m)} - X_K^{(m)})$$

minimum of  $|\theta_{K,L} - \frac{1}{2}|$  with  $\theta_{K,L} \in [0,1]$  and  $\theta_{K,L}V_{K,L} + D_{KL} \ge 0$ ,  $(1 - \theta_{K,L})V_{K,L} - D_{KL} \le 0$ 

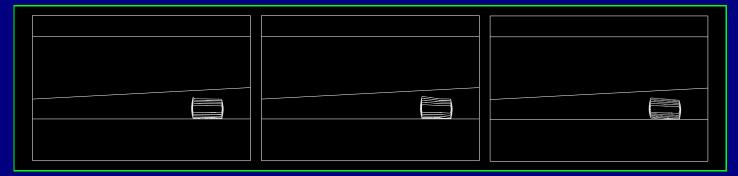


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## **Contour levels of iodine at** 10110 years



MUSCL exp. (left), up.imp. (middle), Péc.imp. (right)



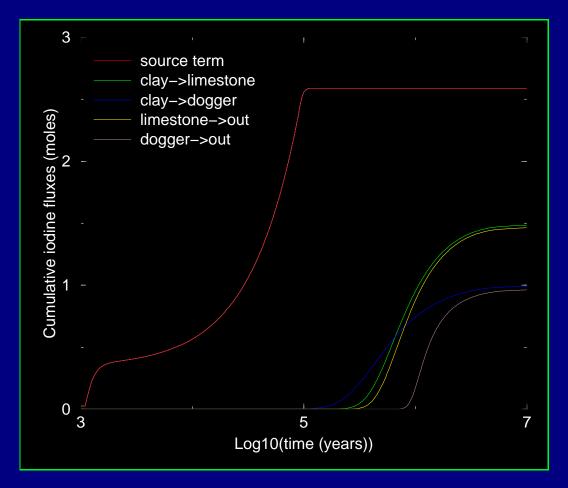
## **Contour levels of iodine at** 50110 years



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#### **Cumulative total fluxes of iodine**





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# **Concluding remarks**

- 1. FV simple and accurate = industrial schemes.
- 2. A complete engineering approach ? Handling uncertainties on
  - (a) porosity, permeability, diffusivity fields, source terms,
  - (b) boundary conditions as function of time.